



Optimal Control of Robotic Wheelchair

SE 514 Term Project

By

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Outline

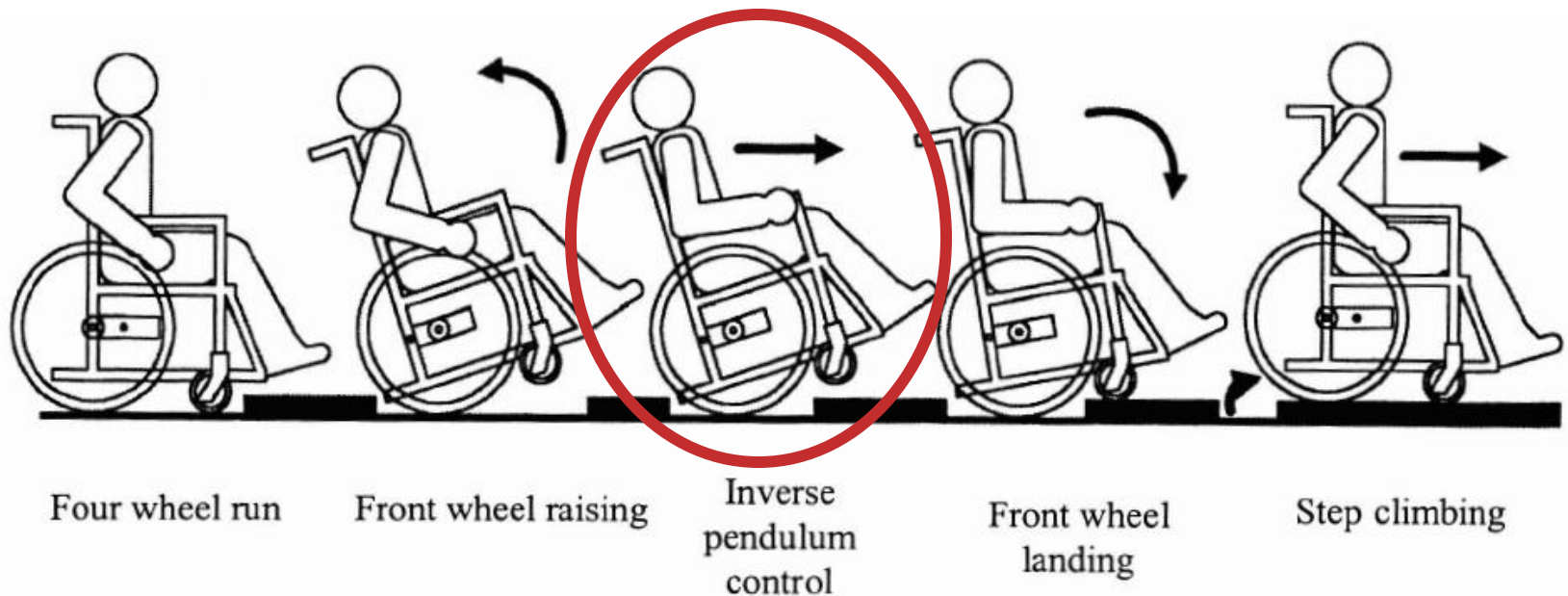
- **Project Overview**
 - Original Work
 - Physical Description
- **Model Discussion**
 - State-Space Model
- **Control & Results**
- **Comments**

Project Overview

- Authors

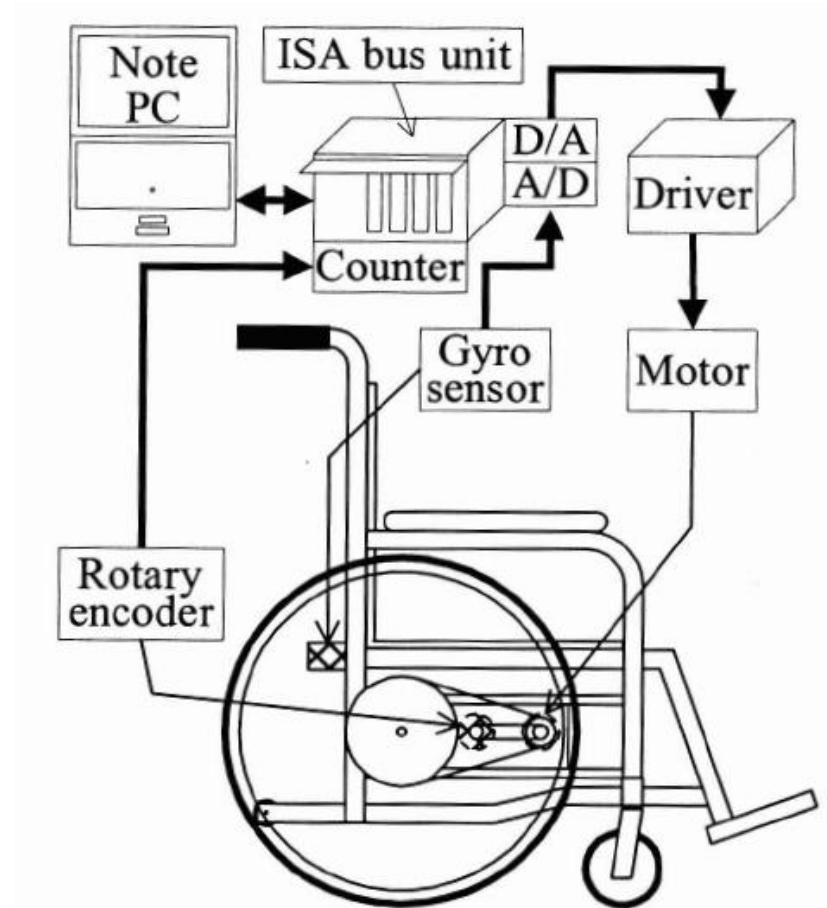
- Yoshihiko Takahashi, Kanagawa Institute of Technology
- Otsushiro Tsubouchi, Kanagawa Institute of Technology

- Idea



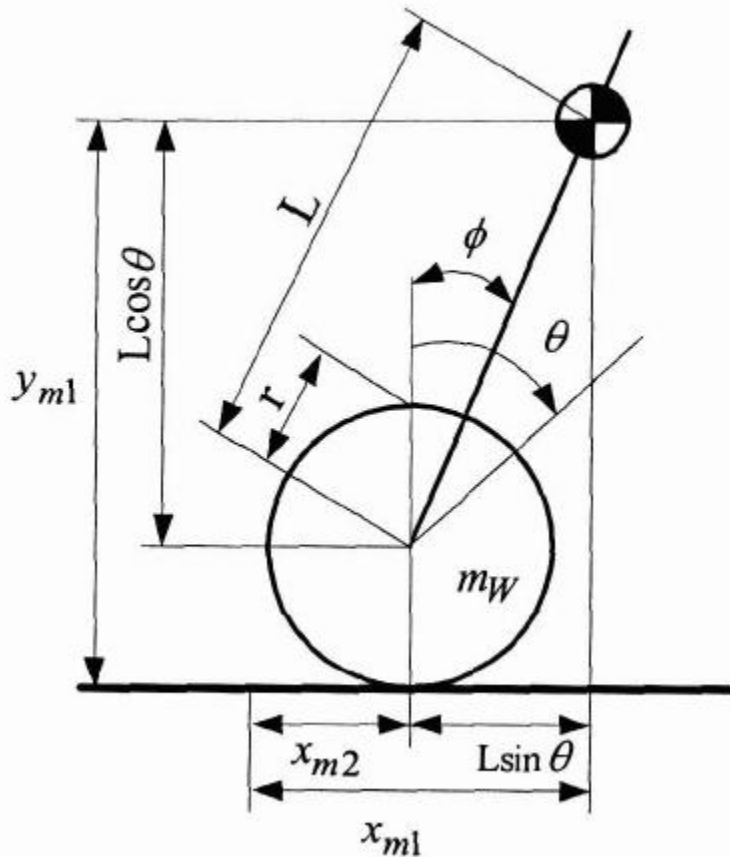
Project Overview

- Hardware Operation
 1. Gyro Sensor: Inclination velocity
 2. Inclination velocity integrated in PC to give wheelchair inclination
 3. $\text{Error} = \text{Inclination} - \text{desired value}$
 4. Error go to Controller
 5. Controller output go to DC Motor



Model Discussion

- Wheelchair Dynamics



ϕ : Body inclination

θ : Wheel rotation

m_W : Mass of wheel

m_B : Mass of body

r : Radius of wheel

k_{cs} : Damping factor of wheel

k_{cf} : Damping factor of shaft

x_{m1}, y_{m1} : Displacement of body

x_{m2} : Displacement of wheel

L : Length between center of gravity and shaft

J_w : Inertia of wheel

J_B : Inertia of body

J_m : Inertia of motor

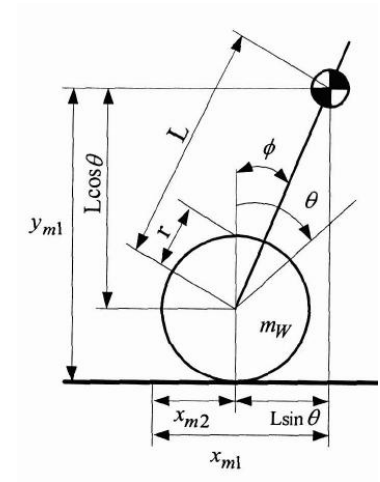
Model Discussion

- Linearization:

- Inverted Pendulum: around $\phi = 0, \dot{\phi} = 0$

- $\Rightarrow \sin(\phi) = \phi$

- $\Rightarrow \cos(\phi) = 1$



Model Discussion

- Differential Equations

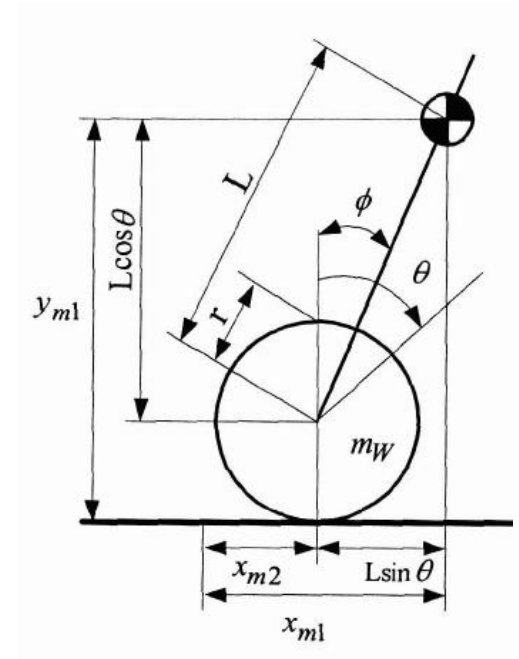
$$\left(M_b L^2 + J_b + J_m K_g^2\right) \ddot{\phi} + \left(M_b r L - J_m K_g^2\right) \ddot{\theta} + K_{cs} (\dot{\phi} - \dot{\theta}) - M_b g L \phi = -\frac{K_g K_t}{R} v$$

$$\left(M_b r L - J_m K_g^2\right) \ddot{\phi} + \left\{ (M_w + M_b) r^2 + J_w + J_M K_G^2 \right\} \ddot{\theta} - K_{cs} \dot{\phi} + (K_{cs} + K_{cf}) \dot{\theta} = \frac{K_g K_t}{R} v$$

- ϕ : Inclination of chair (rad)
- θ : Wheels rotation (rad)
- M_b : Mass of chair & person (kg)
- L : length between wheelchair shaft & center of gravity (m)
- J_b : Inertia of chair & person (kg.m²)
- J_m : Inertia of DC motor (kg.m²)
- K_g : Gear Ratio
- r : wheel radius (m)
- K_{cs} : wheel shaft damping (N.m/(rad/sec))
- K_t : Torque constant of motor (N.m/A)
- J_w : Inertia of wheels (kg.m²)
- M_w : Mass of wheels (kg)
- K_{cf} : Damping between floor & wheels (N.m/(rad/sec))

Model Discussion

- $M_b = 84.16 \text{ kg}$
- $L = 0.29 \text{ m}$
- $J_b = 29.3 \text{ kg.m}^2$
- $J_m = 7.0 \times 10^{-6} \text{ kg.m}^2$
- $K_g = 772$
- $r = 0.305 \text{ m}$
- $K_{cs} = 12.3 \text{ N.m}/(\text{rad}/\text{sec})$
- $K_t = 0.0239 \text{ N.m}/\text{A}$
- $J_w = 0.11 \text{ kg.m}^2$
- $M_w = 6.52 \text{ kg}$
- $K_{cf} = 8.78 \text{ N.m}/(\text{rad}/\text{sec})$
- $R = 0.84 \text{ ohm}$



Model Discussion

- State-Space Model

$$\begin{bmatrix} \dot{\phi} \\ \dot{\theta} \\ \ddot{\phi} \\ \ddot{\theta} \end{bmatrix} = \begin{bmatrix} 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \\ 6.0236 & 0 & -0.3895 & 0.4464 \\ -1.5498 & 0 & 1.0674 & -1.7724 \end{bmatrix} \begin{bmatrix} \phi \\ \theta \\ \dot{\phi} \\ \dot{\theta} \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ -0.6955 \\ 1.9061 \end{bmatrix} v + \begin{bmatrix} 0.09 \\ 0.025 \\ 0.075 \\ 0.05 \end{bmatrix} w$$

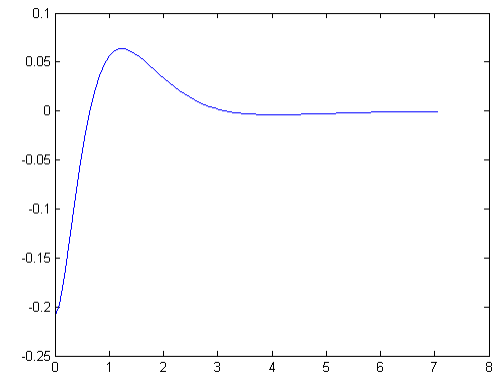
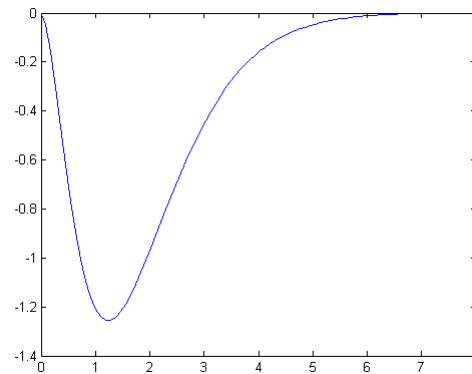
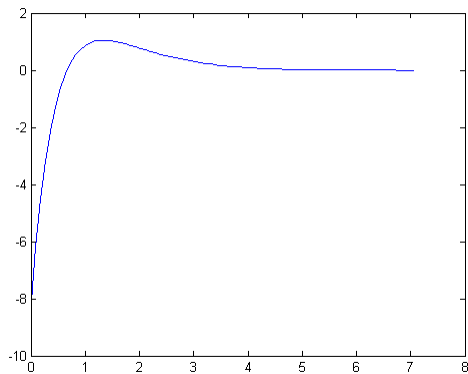
$$\begin{bmatrix} \phi - \theta \\ \dot{\phi} \end{bmatrix} = \begin{bmatrix} 1 & -1 & 0 & 0 \\ 0 & 0 & 1 & 0 \end{bmatrix} \begin{bmatrix} \phi \\ \theta \\ \dot{\phi} \\ \dot{\theta} \end{bmatrix} \quad z = \phi = [1 \quad 0 \quad 0 \quad 0] \begin{bmatrix} \phi \\ \theta \\ \dot{\phi} \\ \dot{\theta} \end{bmatrix}$$

$$x_0 = \begin{bmatrix} -0.21 \\ 0 \\ 0 \\ 0 \end{bmatrix} \text{ rad} \Leftrightarrow \phi_0 = -12^\circ$$

LQR

- 1)

$$Q = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix}, R = 1$$

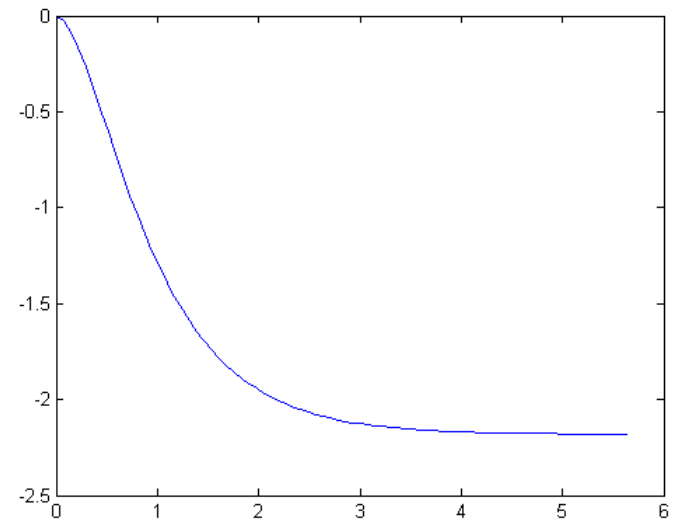
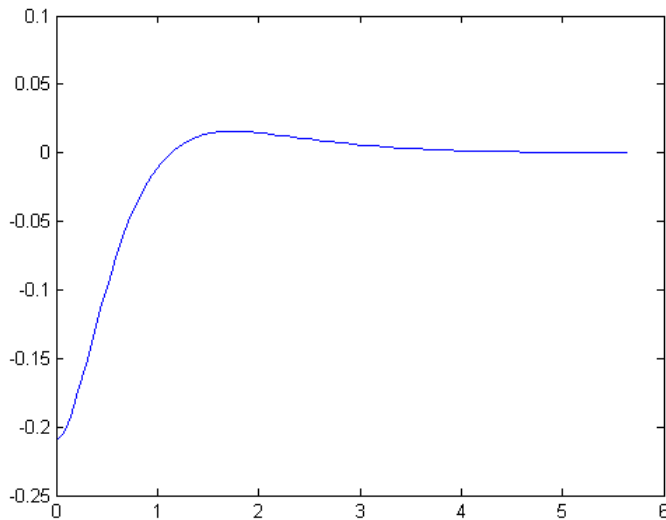


- Increasing weight on ϕ have no effect

LQR

• 2)

$$Q = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix}, R = 1$$

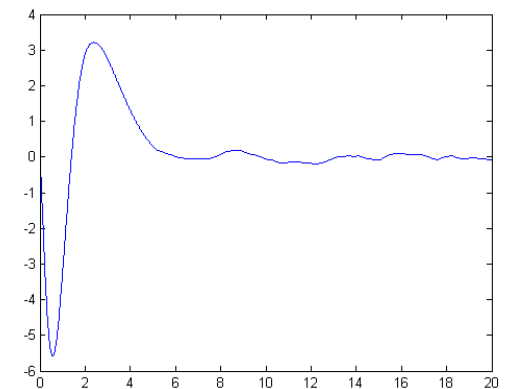
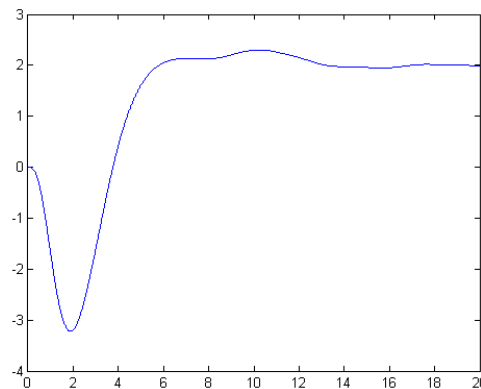
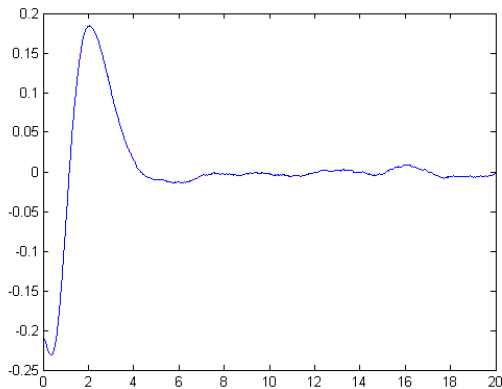


- Little overshoot in ϕ
- No need for Wheel rotation θ to be zero!
- somehow faster settling

LQG

• 1)

$$Q = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix}, R = 1$$

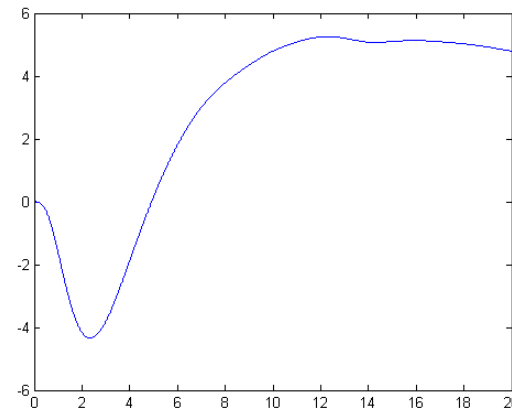
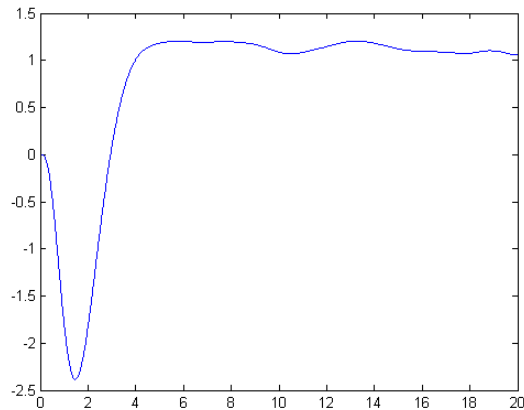
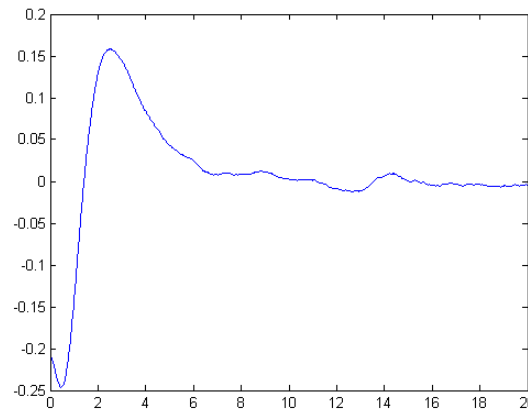
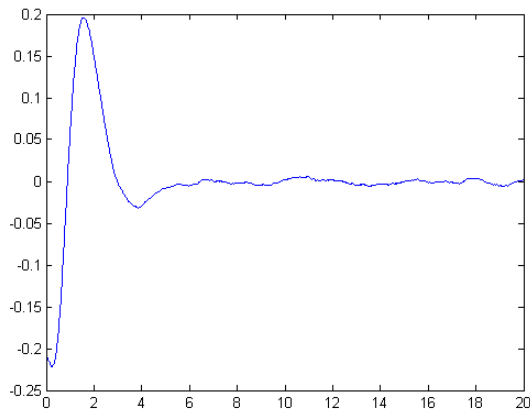


- Relatively high overshoot in ϕ
- Wheel rotation needs time to back to zero

LQG

• 2)

$$Q = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix}, R = 0.1, 10$$

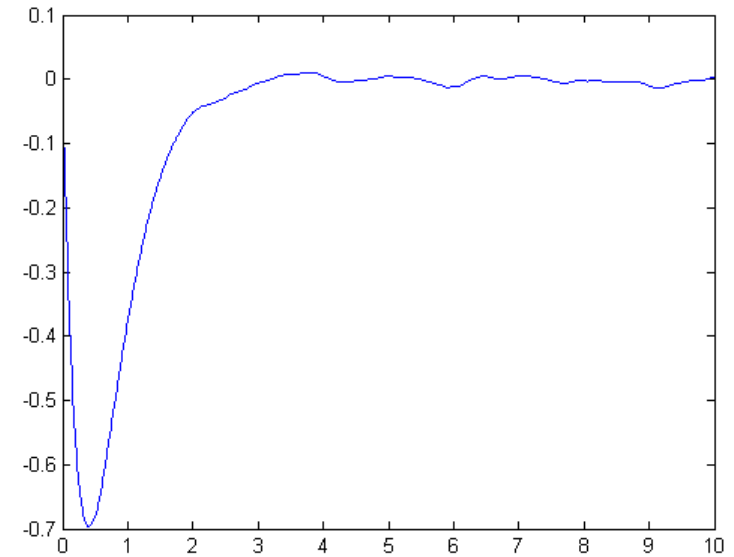
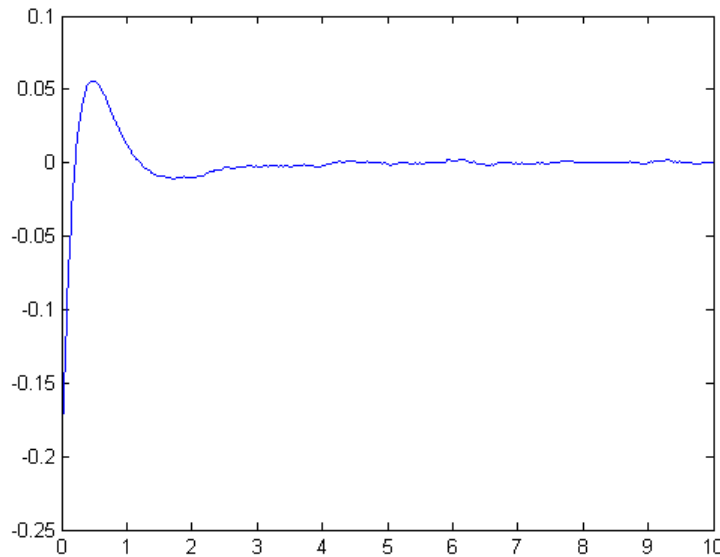


- Decreasing weight on input do not change much

- increasing R improves performance with smaller overshoot

- more weight on input \Rightarrow acceptable current values \Rightarrow but longer settling time

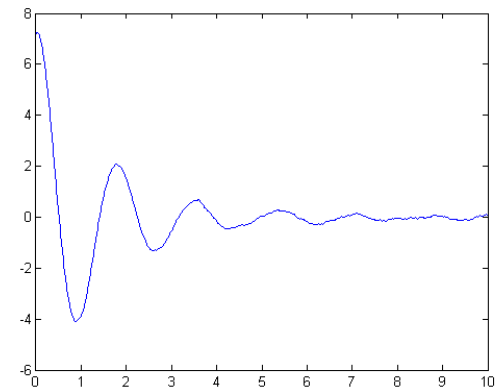
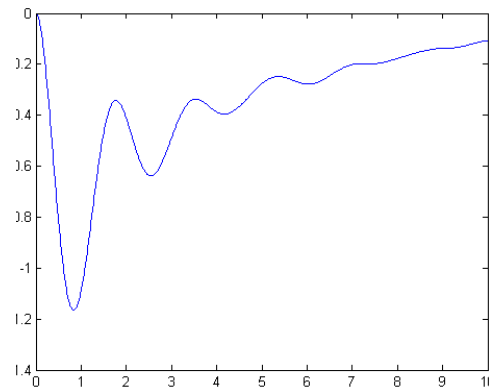
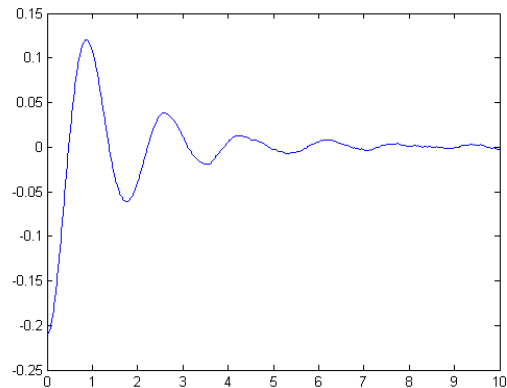
H2 Control



- Faster response & smaller overshoot
- No control input constraint \Rightarrow huge input jump ($\sim 2.5 \times 10^7$ A)
- So, boundary on minimization of H2-norm:
 - No change in responses
 - No change in control input behavior

H_∞ Control

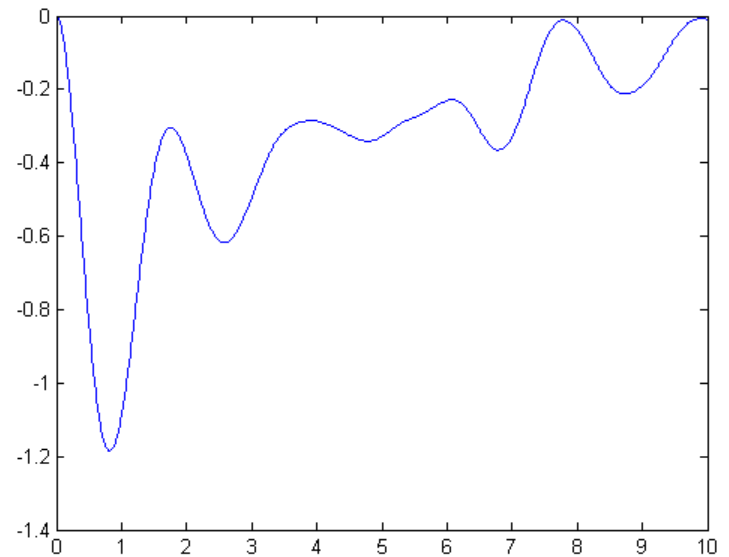
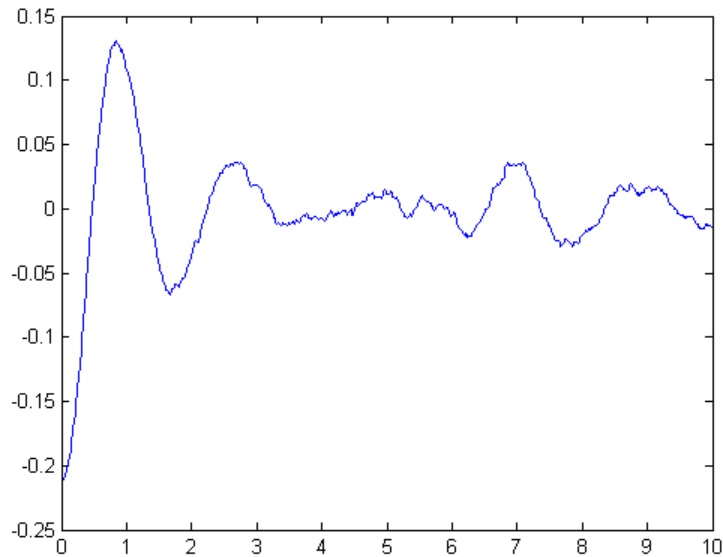
- Same problem for control input
- But trying to minimize γ subject to $\gamma > 0.5$



- oscillatory behavior on ϕ

H_∞ Control

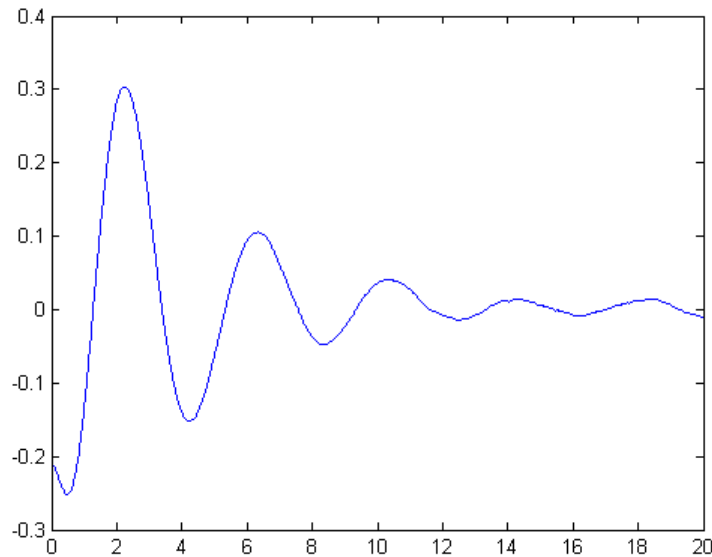
- Making noise 5 times bigger



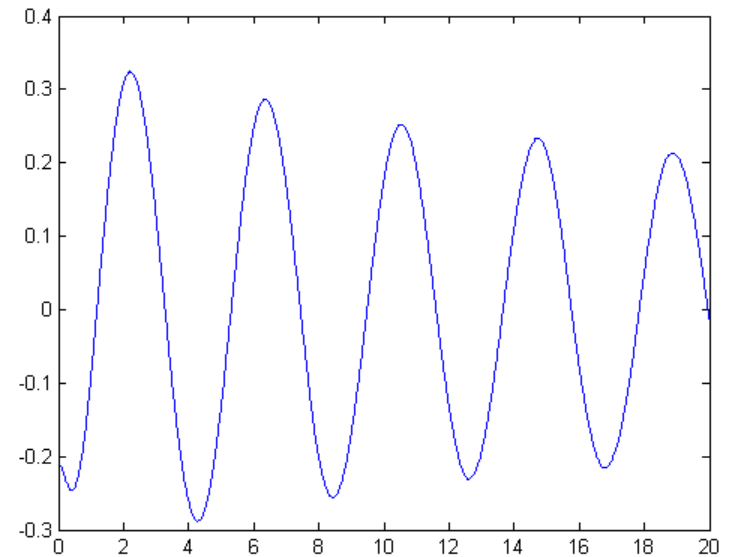
Changes in Physical System

- Using the same LQG design and resulting K
- But:

Wheelchair & body mass increased by 20%



wheel radius 31 to 40 cm



General Comments

- Best practical & acceptable performance:
 - LQG: $R=10$ (or more) and unit weight on ϕ , θ
 - more weight on input \Rightarrow acceptable current values \Rightarrow but longer settling time
 - Acceptable overshoot (~ 0.15 rad), settling time (~ 5 sec) and control input behavior (maximum ~ 2.5 A)
- In general, inverted pendulum control is OK when ϕ is almost zero. So, big inclinations will need other ways of control

End of Presentation

- Questions R Welcomed