KFUPM SE 513 – Modeling & Systems Identification Course Project

#### **Identification of a Magnetic Levitation System**

#### For Prof. Doraiswami

By

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#### **Maglev Trains**



JR-Maglev MLX01 reached 581 km/h (Japan)

superconducting magnets which allow for a larger gap, and repulsive-type Electro-Dynamic Suspension (EDS).

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#### **Magnetic Bearings**



-support moving machinery without physical contact

- advantages include very low and predictable friction, ability to run without lubrication and in a vacuum

- industrial machines such as compressors, turbines, pumps, motors and generators

#### **Research Experimentation**





## Outline

#### 1. System Dynamic Model

- 1. Nonlinear Model
- 2. Linearized Model

#### 2. System in the LAB

- 1. Feedback<sup>®</sup> MAGLEV System
- 2. Control Loop

#### 3. Experiment

- 1. Hardware
- 2. Software
- 3. Data

#### 4. Identification

- 1. Models
- 2. Results
- 3. Analysis

#### 5. Future Directions

#### System Model

#### **References** for Model:

1- P. S. Shiakolas, R. S. Van Schenck, D. Piyabongkarn, and I. Frangeskou, "Magnetic Levitation Hardware in the Loop and MATLAB Based Experiments for Reinforcement of Neural Network Control Concepts", IEEE Transactions on Education, 2004

2- A. Bittar and R. M. Sales, "H2 and H, control applied to an electromagnetically levitated vehicle", IEEE International Conference on Control Applications, Connecticut, USA, 1997

#### **Free-Body Diagram**



#### **Free-Body Diagram**



L(x) Total Inductance

 $L_0 X_0$  Operating Points

 $L_{\text{JUNE $2008}}$  Coil Inductance

## **Free-Body Diagram**

Input: Voltage / Output: Ball Position

$$M\ddot{x} = Mg - K_L \frac{i^2}{x^2}$$
with  $V = R_c i + L_c \frac{di}{dt} \cong K_c i$ 
Assume no dynamics



 $R_c$  Coil Resistance

/ Input: Voltage

#### **Nonlinear Model**

$$\ddot{x} = g - \frac{K_L K_c^2 V^2}{M x^2}$$

$$\ddot{x} = g - K_s \frac{V^2}{x^2}$$
Input: Voltage / Output: Ball Position

#### Linearization

$$\ddot{x} = g - K_s \frac{V^2}{x^2}$$

 $\ddot{x} = f(x, V)$ 

For some Operating Points  $X_0$  ,  $V_0$ 

 $\cdot V$ 

$$\ddot{x} = \frac{\partial f}{\partial x}\Big|_{X_0, V_0} \cdot x + \frac{\partial f}{\partial V}\Big|_{X_0, V_0}$$

$$\ddot{x} = \frac{2K_s V_0^2}{X_0^3} x - \frac{2K_s V_0}{X_0^2} V$$

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#### **Transfer Function**

$$\ddot{x} = \frac{2K_s V_0^2}{X_0^3} x - \frac{2K_s V_0}{X_0^2} V$$

$$\frac{x(s)}{V(s)} = \frac{\frac{(-2K_sV_0)}{X_0^2}}{(S^2 - \frac{2K_sV_0^2}{X_0^3})}$$

So, 
$$\frac{x(s)}{V(s)} = \frac{b}{(s^2 + a^2)}$$

#### 2<sup>nd</sup> order system

## **MAGLEV** in Lab

- In closed-loop
- Photosensor (IR) for position
  - Sensor = 2.5V -> furthest from magnet
  - Sensor = -2.5 -> closest to magnet
- Set-point manually changed
- Analog Controller onboard



#### **Closed-Loop System**



Controller



Lead/Lag Compensator



## Experiment



#### Software

- Collected data Using:
   "VI Logger"
- Data-logging software
- Scheduling features
- Flexible adjustments
- Choose sampling speed

- Disturbance Generation:
   "LabVIEW"
- You can generate any kind of signals as required:
  - Random Sequence,
  - sinusoids,
  - Etc

#### Data

- Three set-points:
  - 0, 1, -1
- Sampling rate:
  - 1kHz, i.e. 1000 samples per second
- Disturbance = Random Sequence with small amplitude
- Data Collected for:
  - Disturbance (d)
  - System Output (x)
  - Control Input (V)

#### Data

- Data(0) = 3 × 41431 samples
- Data(1) = 3 × 41309 samples
- Data(-1) = 3 × 39257 samples



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## SYSTEM IDENTIFICATION

#### **Model Structure**

Recall

$$\frac{x(s)}{V(s)} = \frac{b}{(s^2 + a^2)}$$

• Due to discretization

$$G(z) = \frac{b_0 + b_1 z^{-1}}{1 + a_1 z^{-1} + a_2 z^{-2}}$$

## **Other Information**

- As hardware sampling period is 1ms
  - we can artificially enlarge the sampling period by 'skipping' samples
- Convenient speeds 1~10ms
- It is expected to have:
  - Poles around unit circle

#### **MAGLEV Identification**

• Open-loop System Input: V, Output: x

$$G_0(z) = \frac{4.869 \times 10^{-5} + 0.0001446z^{-1}}{1 - 1.899z^{-1} + 0.8996z^{-2}}$$

$$G_1(z) = \frac{-2.9 \times 10^{-6} + 0.0001233z^{-1}}{1 - 1.837z^{-1} + 0.8374z^{-2}}$$

$$G_{-1}(z) = \frac{4.37 \times 10^{-5} + 0.0001342z^{-1}}{1 - 1.911z^{-1} + 0.911z^{-2}}$$

#### **Results Plots**



Samples 2000-3000 showing

Set-point = 0

Set-point = 1

Set-point = -1

#### **Results Analysis**

- System 1 Poles:
  - 0.9932, 0.9057
- System 2 Poles:
  - 0.9968, 0.8401
- System 3 Poles:
  - **0.9958**, 0.9148

• All poles proved to be near the unit circle

## **Identification Approach 2**

• Here, lets make

$$G(z) = \frac{b_0 + b_1 z^{-1}}{1 + a_1 z^{-1} + z^{-2}}$$
$$a_2 = 1$$

• To make poles *exactly* at the unit circle

$$y(k) + y(k-2) = -a_1y(k-1) + b_ou(k) + b_1u(k-1)$$

$$unknown parameters$$

• Y & A matrices will be different

#### **Results 2**

• Tested for Set-Point 0,

$$G_0(z) = \frac{4.534 \times 10^{-5} + 0.0001398z^{-1}}{1 - 1.999z^{-1} + z^{-2}}$$

• Poles

 $0.9997 \pm j 0.0257 \rightarrow |0.9997 \pm j 0.0257| = 1$ 



## **Closed-Loop Identification**

• Input: *Disturbance*, Output: *x* 

$$G_{CL}(z) = \frac{0.00296 + 8.902 \times 10^{-5} z^{-1}}{1 - 2.289 z^{-1} + 1.723 z^{-2} - 0.4331 z^{-3}}$$

• Poles

• Controller should be tuned!

## **Future Directions**

- Horizontal Motion Dynamics
  - Maybe need of another sensor
  - Or, observable model -> Horizontal motion can be estimated
- Going to Continuous-time Analysis:
  - Study effect of discretization
- Improve Controller Design
  - More stable design



## **Final Remarks**

- Acknowledgement:
  - Thanks for Prof. Doraiswami for constant advising
- Interesting Project!
  - Included many concepts together: Modeling, Magnetic Fields, Opamps, Nonlinearities, Numerical Methods, LabVIEW, Discrete-time Analysis, and of course Identification, etc.

## THANKS!

# •Q&A